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# Novel Ultrasonic Horn Designs for Extraterrestrial Applications

# **Stewart Sherrit** Jet Propulsion Laboratory, Caltech April 18,2012

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### Outline

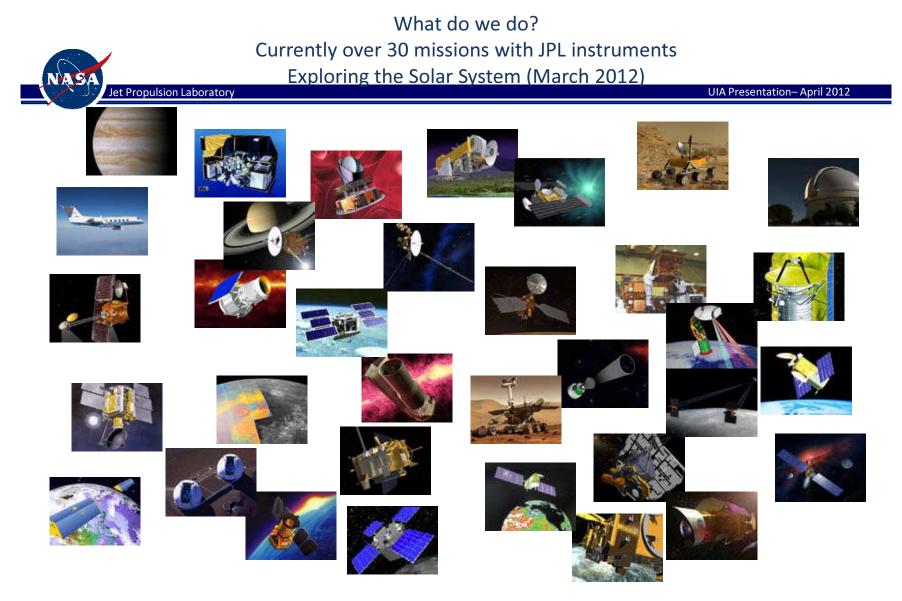
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•What does JPL do?

• Who are we?

•What we do!

Chronology of Sampling technology development
Lithotripsy
Ultrasonic Sonic Driller Corer USDC
USDC –Ultrasonic Rock Abrasion Tool (URAT)
Inverted Stepped Horns
Folded Horns
Flipped horns
Dog Bone Horns
Flexure Monolithic Horns
Asymmetrically grooved horns



See - http://www.jpl.nasa.gov/missions/index.cfm?type=current

### Example of a current Mission at JPL!



### http://mars.jpl.nasa.gov/msl/multimedia/videos/index.cfm?v=24



Compilation of Physicists and Mechanical Engineers with backgrounds in Ultrasonics, Mechanisms, Piezoelectrics, NDE, Dynamics

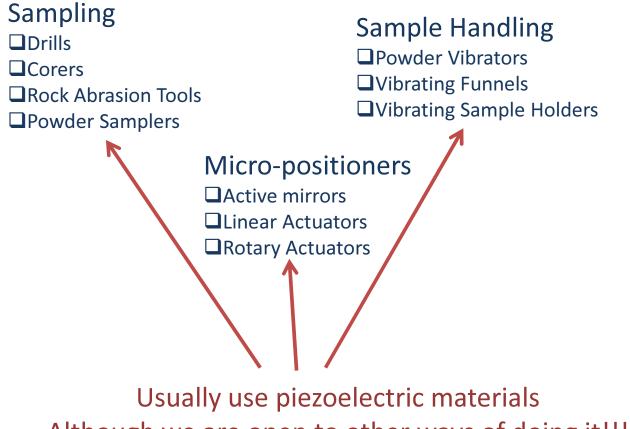


http://ndeaa.jpl.nasa.gov

### What we do: Our Niche



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Although we are open to other ways of doing it!!!

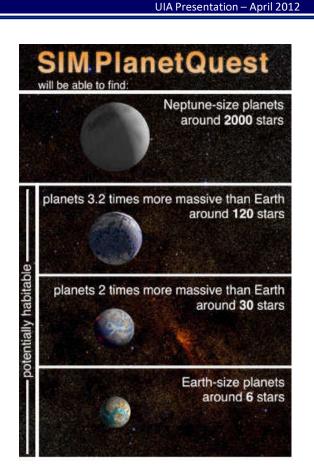
# Micro-positioners eg. Space Interferometry Mission

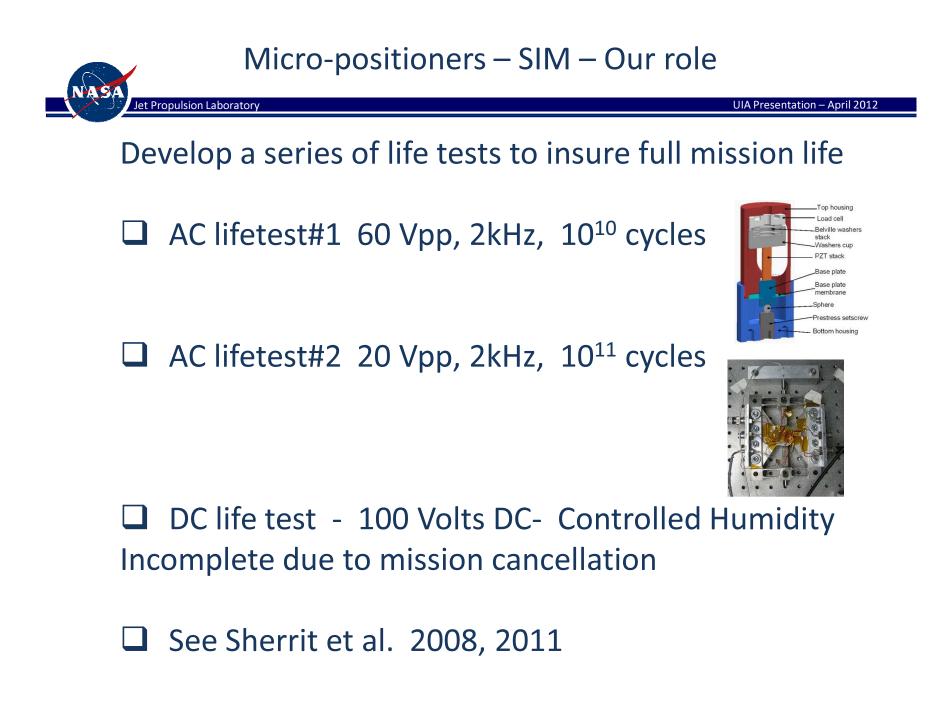




- •3 interferometers
- •2x7.2 and 9 m baselines
- Earth trailing solar orbit
- 5.5 year mission life with goal of 10 years
- Over 200 piezoelectric stacks





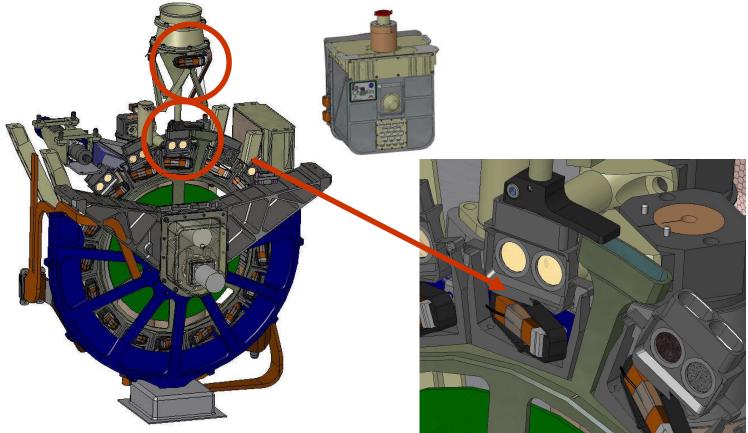


MSL Instrument - CHEMIN – XRD XRF – Sample cell shaker and inlet funnel



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Original Design- problems at Mars ambient and under launch random vibe.



## Sample Handling – Our Role

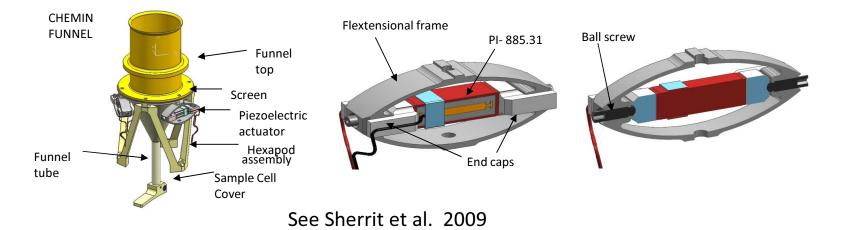


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MSL has 21 piezoelectric actuators for sample handling and instrument cells

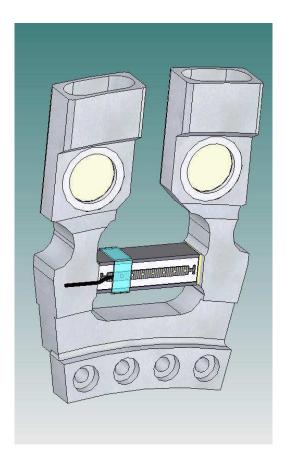
- 2 on SAM inlet funnel
- 3 on CHEMIN inlet funnel for powder delivery assist
- 16 on CHEMIN instrument sample wheel



### Sample Handling – Our Role



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#### MSL Sample cell Shakers Re-design

Phillippe Sarrazin (Inxitu) came up with tuning fork design and with Eric Olds (Swales) they came up with

#### Problems

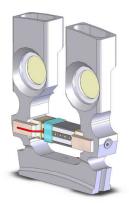
1/ Thermal analysis showed marginal thermal stress on piezoelectric2/ Wheel mounting created anisotropic stress. (Energy to wheel)

### Sample Handling – Our Role



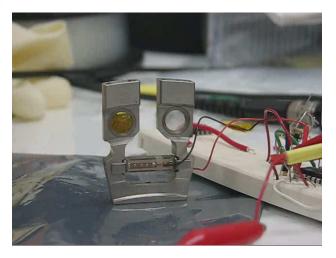
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### MSL Sample cell Shakers Re-design fine tuning -



### Solutions

- 1/ Shorten Piezoelectric
- 2/ Use Invar end caps
- 3/ Use ball/set screw mount
- 4/ Soften Tuning fork
- 5/ make base symmetric



See http://msl-scicorner.jpl.nasa.gov/Instruments/CheMin/

# Sampling

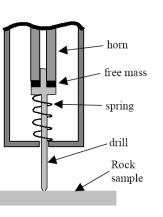
Started out looking at pure ultrasonics with Cybersonics Inc. (Erie, PA) Discussions with Cybersonics Inc. led to the development of the USDC



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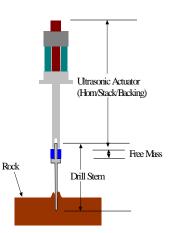


Figure 8. Schematic cross section of the drill assembly with restoring spring and impedance matching mass.

First paper describing the technology - see Sherrit et al. (1999)



Initial development was mainly experimental- looking at ways to improve or expand the technology.



http://www.youtube.com/watch?v=phLiWya1sGo

First real engineering occurred when USDC was selected (URAT) for backup Rock Abrasion Tool on the Mars Exploration Rovers (MER)



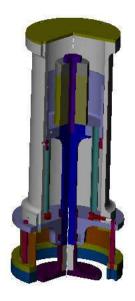
# Sampling

(URAT) Ultrasonic Rock Abrasion Tool -Mechanical design and fabrication along with flight like electronics (FPGA switching H-bridge)



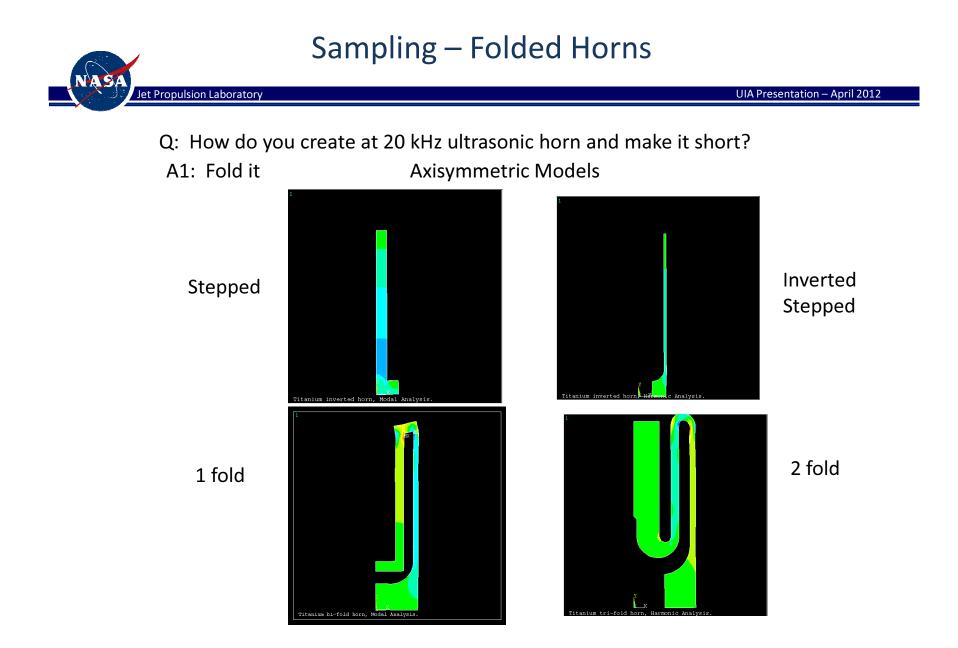






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The initial response was, "This is great. Can you make it Shorter?" Which is how we started to develop novel Ultrasonic horns

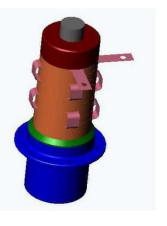


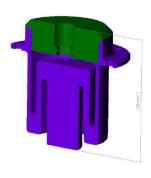


# Sampling – Folded Horns

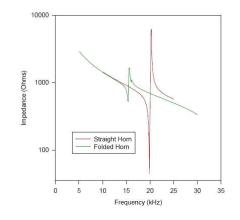
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Design and tested the doubly Folded horn-











## Sampling – Folded Horns

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### Incorporated the horn in a non-pneumatic rock powder sampler





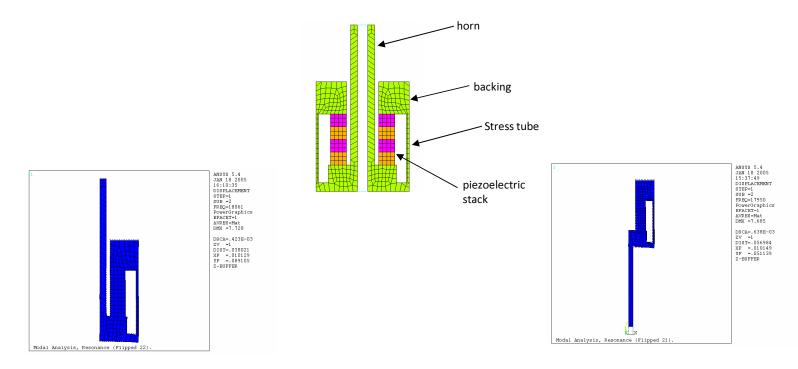
We also came up with a solid planar Monolithic version. See Sherrit et al. 2002







## Sampling – Flipped Horns

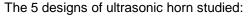


	Flipped horn	Standard horn	Difference (%)
Resonance frequency (Hz)	18061	17950	0.61
Horn-tip disp. (m), 1 volt	4.62×10 <sup>-7</sup>	4.63×10-7	0.22
Electric current (amp), 1 volt	1.05×10 <sup>-2</sup>	1.04×10 <sup>-2</sup>	0.95
Max. stress (Pa), 1 volt	$2.50 \times 10^{6}$	2.24×10 <sup>6</sup>	10.4
Horn-tip disp. (m), 1 watt	4.51×10 <sup>-6</sup>	4.54×10 <sup>-6</sup>	0.67

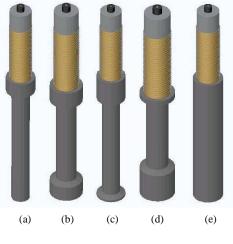
Table 1. Comparison of performance of the flipped and the standard horns. See Chang et al. 2005



For an impact device the interaction time is of the order of 50  $\mu$ s Which suggest at the tip for maximum momentum transfer the tip Thickness should be less than  $\approx$  50  $\mu$ s \*4000 m/s = 0.02 m



- a) Conventional
- b) Neck at middle span of horn
- c) Neck moved down 20 mm
- d) Neck moved up 20 mm
- e) No neck



Horn Type	Horn length (mm)	Resonance (Hz)	Anti-Resonance (Hz)	Coupling Factor	Max. Displacement
					(mm)
Conventional	250	5314	5726	0.372	0.209
Neck at middle	200	5473	5947	0.391	0.185
Neck up 20 mm	175	5421	5916	0.400	0.185
Neck down 20 mm	255	5266	5666	0.369	0.209
No Neck	240	5304	6016	0.472	0.133

See Chang et al. 2004



# Sampling – Dog-bone Horns Analytical Modeling

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Integrated program package: Modal analysis – Resonance Modal analysis – Anti-resonance Harmonic analysis Simplified integrated model Impact analysis Spring-mass model

**Resonance frequency 5195Hz** 



### Sampling – Used Dog-bone Horn to produce Ice gopher Wire-line hammer drill

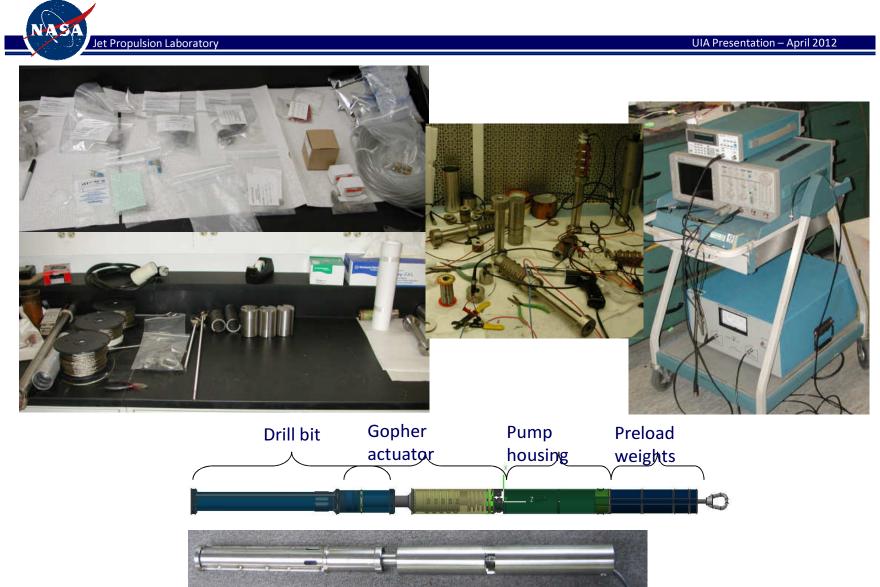
Drill bitGopher transducerPump housingPreload weightsImage: Construction of the state o

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Dog-bone horn PZT stack Backing Stress bolt

Components Gopher Actuator(Transducer) Drill bit Free mass Pump Preload

### **Gopher Design Fabrication**



### Gopher Field Trips – Mt. Hood, Oregon

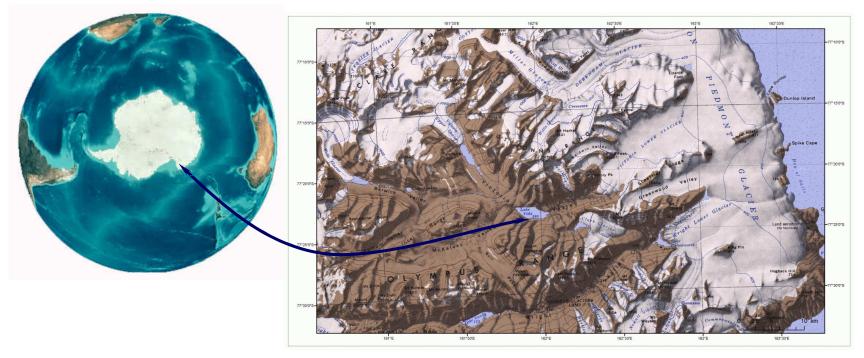




### Gopher Field Trips – Lake Vida, Antarctica



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Lake Vida (77.23°S 162°E) in the McMurdo Dry valleys, Antarctica, offers a Mars analog environment for testing the detection and description of life in a previously unstudied extreme ecosystem







### Gopher Field Trips – Lake Vida, Antarctica







### Gopher Field Trips – Lake Vida, Antarctica







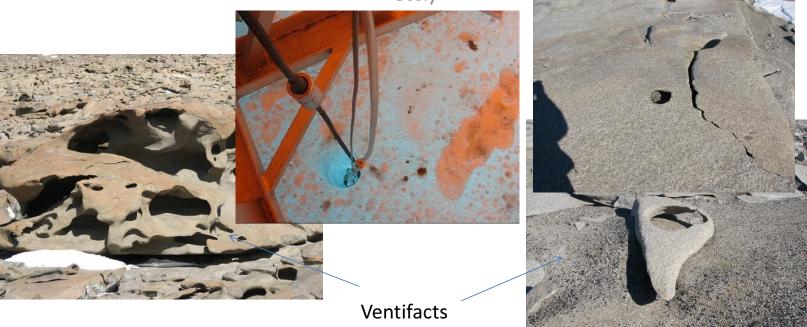
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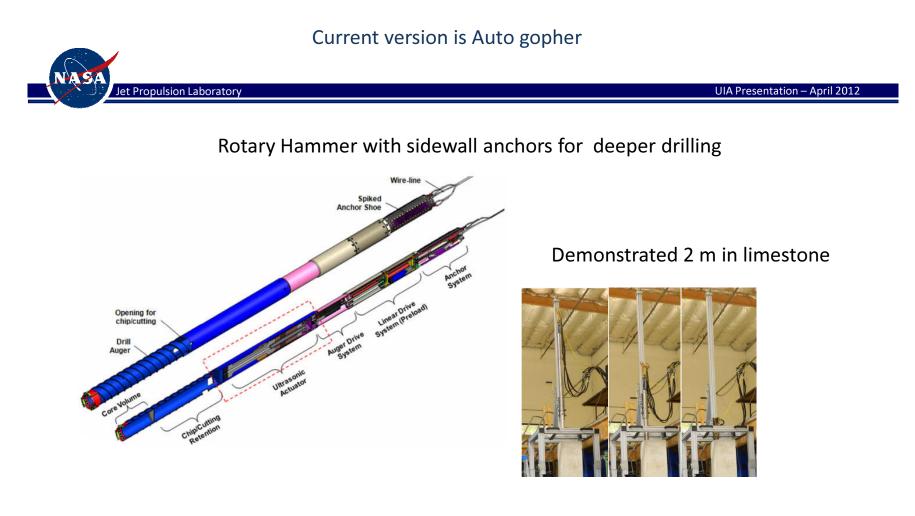


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# Drilling depth of 1.76m is more than the total length of the Gopher including its support elements (pump, preload weights,

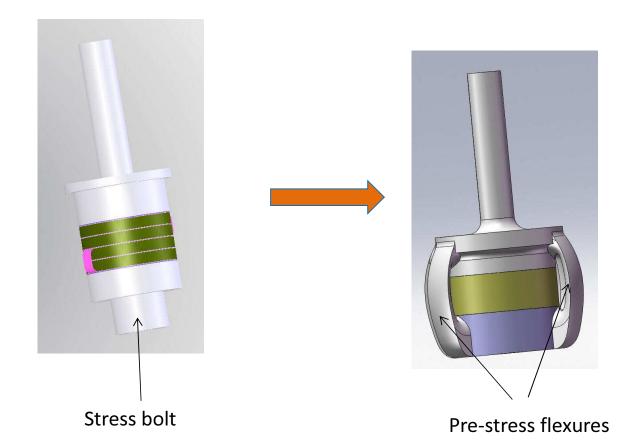
etc.)





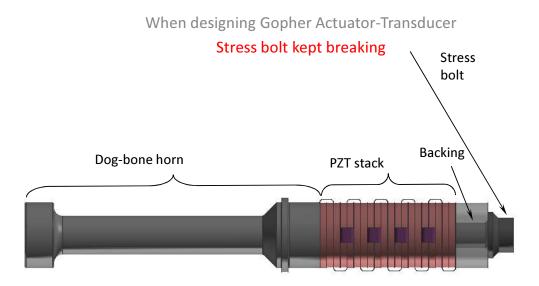
See Bar-Cohen et al. 2012







# Flexured horns: Why?





- 1. Increase manufacturing yield of disks vs rings
- 2. No Internal Discharge to stress bolt
- 3. Higher energy density
- 4. Pre-stress is not limited by bolt diameter
- 5. Actuator has higher coupling since it is not working against stiff bolt
- 6. Softer spring increases thermal preload stability

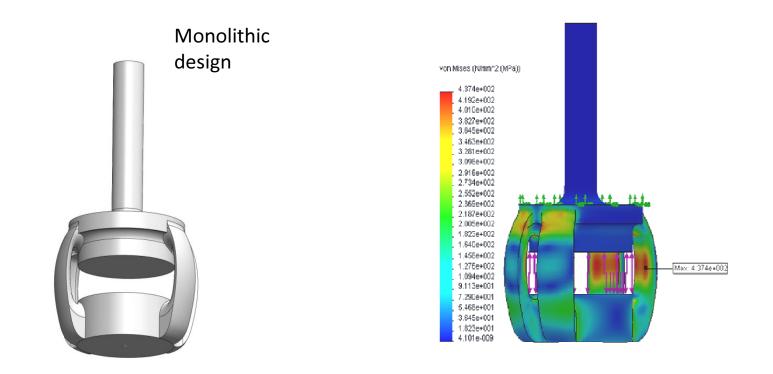


**Bellville Washers** 

High Temperature Drill 500 °C

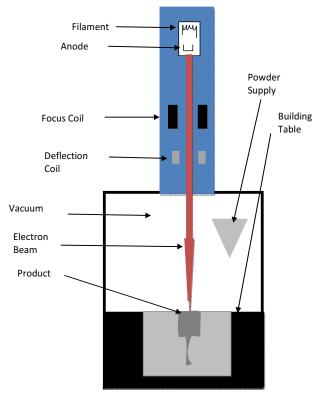
### Design Example







### Chose EBM – Electron Beam Melting CALRAM Inc.



The design is also amenable to investment casting and other low cost high production techniques.

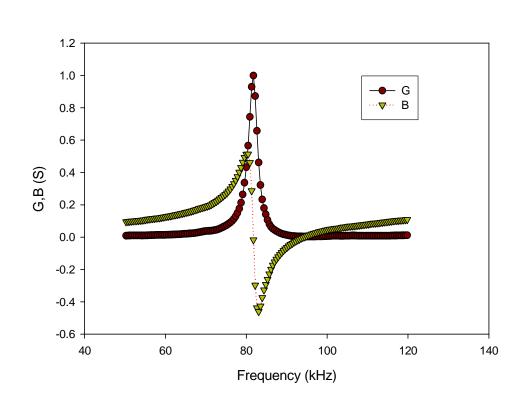
Examples from Arcam AB •Landing gear component •Tri-flange Implant www.arcam.com







Impedance spectra of the bare Piezomechanik Gmbh bipolar stack (9.33 mm, 25.4 OD)





Small signal resonance analysis the bare stack

Material d33eff = 480 pC/N Capacitance C=261 nF. Coupling  $k_{33}$  =0.56 sE33=5.4x10<sup>-11</sup> m<sup>2</sup>/N Q was 30.

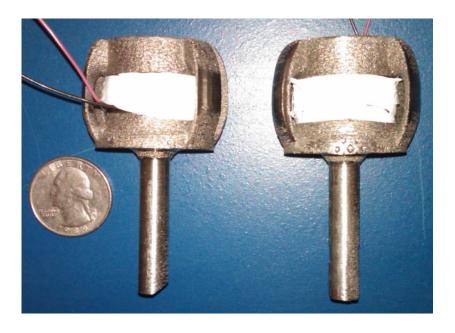


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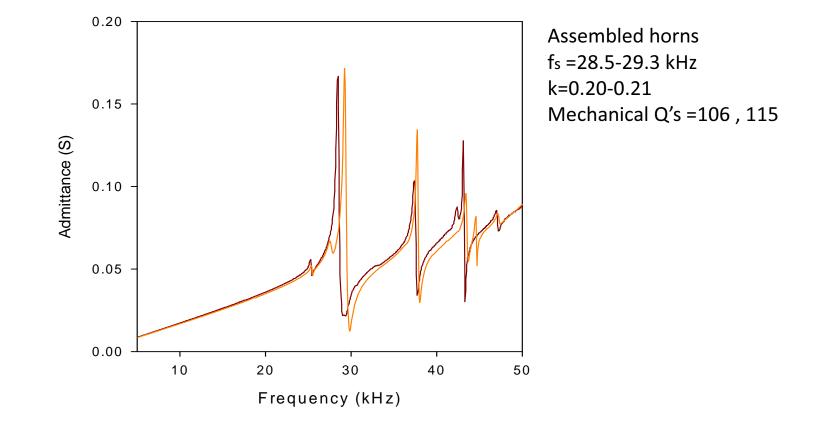
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Inner surfaces were finished using mill
Flexures opened using pre-stress rig
Stacks fixed using 3M 2216
Preload monitored by measuring charge produced when flexures released





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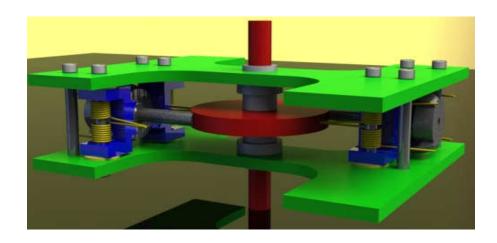




### Example application

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Horns used in Barth Motor





Initial results - 15 RPM at 0.3 N-m





Develop technologies for sample acquisition in extreme environments with reduced power, weight on bit and increased efficiency

- •Hammering is great for breaking rock.
- •Rotation is great for removing cuttings.
- •This is why you have rotary hammer drills at Home depot

Can we develop a piezoelectric mechanism for hammering and with the same piezoelectric actuator induce rotation?

YES



Drilling using Hammering is limited to a few centimeters depth without a debris extraction method. Rotation with augers is beneficial in that it aids drilling and extracts drilling debris.

Previous approaches to induce rotation from extensional motion

•Create a bit with some asymmetry in shaft to induce rotation

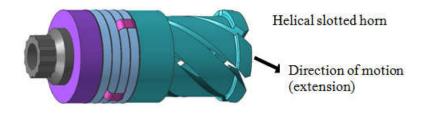
•Impact wrenches/drivers

•Asymmetric teeth on bit



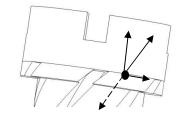
Use existing ultrasonic actuators / horns to create directional impacts on bit.

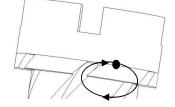
Use the micro-impacts of extension or bending at high frequency to produce macroscopic rotation.



extension



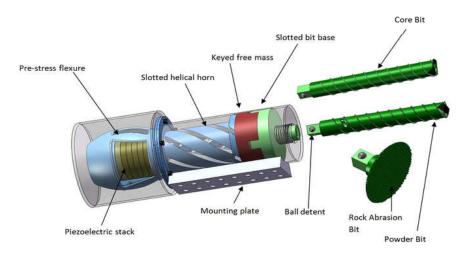






### **Design solution**

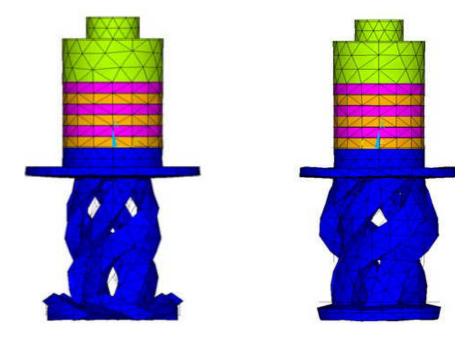
Combine fluted bit rotation (cuttings removal) with Ultrasonic/Sonic percussion (drilled media fracturing and cuttings fluidization)





### Horn Analysis

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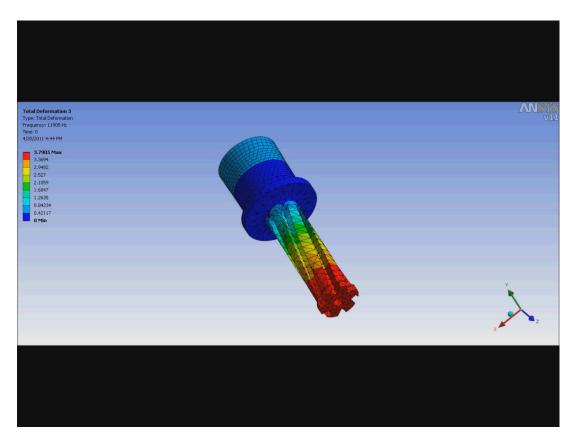


Looked at a large number of horn to produce twist and extension Two rejected horn geometries are shown above.



### An acceptable horn motion

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Frequency, Hz



# Horn Analysis

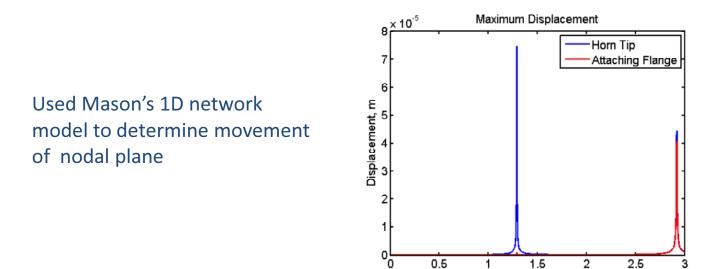
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× 10⁴

#### Harmonic analysis results suggest mode is reasonably coupled

Table 1. ANSYS predicted performance of chosen transducer design at 1 W input power.

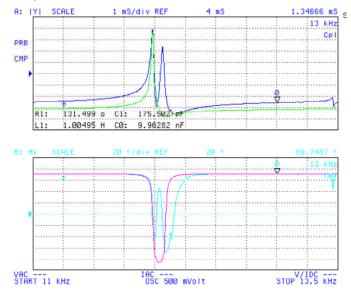
Frequency (First axial	Coupling Coefficient	Tip Displacement,	Tip Rotation, rad	Voltage, V
mode)		μm		
12217	0.08	1.75	4.40E-5	27.0





#### Fabricated horn and tested its frequency response





Transducer performance derived from impedance analysis.

First Resonant Frequency	<b>Electromechanical Coupling Coefficient</b>		
11 972 Hz	0.07		



Testing of the horn tip displacement at resonance. A fotonics fiber optic sensor was used to test both the extension and rotation at the tip at the resonance frequency

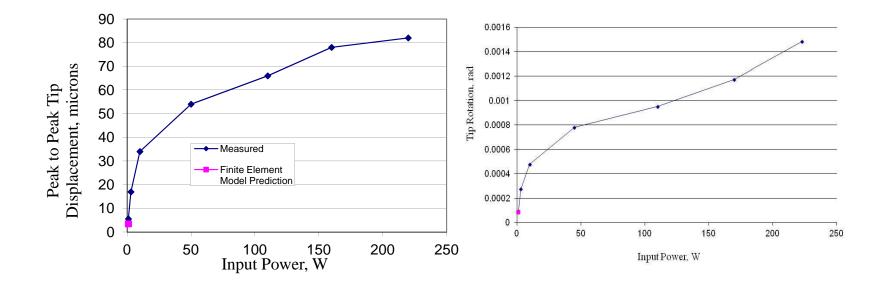




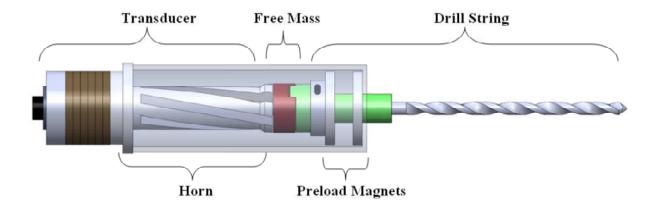
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Comparison of FEM and experimental extension data small signal FEM predictions compare favorably to data at low power

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Impacts on free mass would transmit rotation to bit through key and still be free to expand in the axial direction. The bit and free mass preloaded using NeFeB magnets



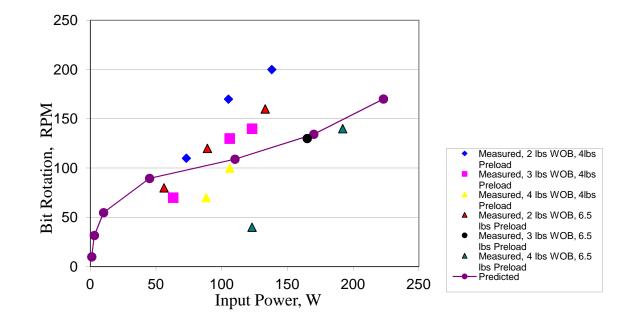
### **Drilling action**

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Also noted at higher frequencies we could rotate in opposite direction





Input Power, W	WOB, lbs	Preload, lbs	Duty Cycle	Drill Rate, mm/min
100	3	4	80 %	8



## Testing

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•A novel horn concept to produce hammering and rotation using a single piezoelectric transducer was investigated theoretically using a variety of modeling methods via MATLAB and ANSYS.

• A transducer design was fabricated and demonstrated simultaneous rotation and hammering.

•This Piezoelectric Rotary Hammer Drill prototype has not been optimized, and requires further development however the un-optimized version rotated at 200 RPM.

•We also noted that we could reverse the direction of rotation by driving at higher frequencies (2x)

•Future work should include considering different horn shape designs, in order to compare with the performance of this initial prototype.

•In addition looking at other geometries, horn materials such as Titanium may aid in increasing the electromechanical mechanical coupling.



# Conclusions

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•Ultrasonic Horns can be designed to produce many original mechanisms.

- •We have just scratched the surface of Potential applications.
- •We are still scratching





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Bar-Cohen, Yoseph (2012) Mircea Badescu, Stewart Sherrit, Kris Zacny, Gale L Paulsen, Luther Beegle, Xiaoqi Bao, "Deep Drilling and Sampling via the Wireline Auto-Gopher Driven by Piezoelectric Percussive Actuator and EM Rotary Motor" Proceedings of the SPIE Smart Structures and Materials/NDE Symposium,vol 8345-78, San Diego, CA, March 12-15

Chang, Z. (2005), S. Sherrit, M. Badescu, X. Bao, and Y. Bar-Cohen, "Design and analysis of ultrasonic actuator in consideration of length reduction for a USDC (Ultrasonic/Sonic Driller/Corer)," Proceeding of the Industrial and Commercial Applications of Smart Structures Technologies, SPIE Smart Structures and Materials Symposium, Paper #5762-10, San Diego, CA, March 7 - 10, 2005.

Chang, Z. (2004), S. Sherrit, X. Bao, Y. Bar-Cohen "Design and analysis of ultrasonic horn for USDC (ultrasonic/sonic driller/corer)", Proceedings of the SPIE Smart Structures Conference, SPIE Paper [5388-34], San Diego, CA., Mar 15-18.

Sherrit, Stewart(2002), Stephen A. Askins, Mike Gradziol, Benjamin P. Dolgin, Xiaoqi Bao, Zensheu Chang, and Yoseph Bar-Cohen, "Novel Horn Designs for Ultrasonic/Sonic Cleaning Welding, Soldering, Cutting and Drilling," Paper 4701-34, Proceedings of the SPIE Smart Structures and Materials Symposium, San Diego, CA, March 17-19

Sherrit, Stewart (1999), B.P. Dolgin, Y. Bar-Cohen, D. Pal, J. Kroh, T. Peterson "Modeling of Horns for Sonic/Ultrasonic Applications", Proceedings of the IEEE Ultrasonics Symposium, pp. 647-651, Lake Tahoe, Oct 1999

Sherrit, Stewart (2008), Christopher M. Jones, Jack B. Aldrich, Chad Blodget, Xiaoqi Bao, Mircea Badescu, Yoseph Bar-Cohen, "Multilayer piezoelectric stack actuator characterization", Proceedings of the SPIE 15th International Symposium on Smart Structures and Materials, San Diego, CA, SPIE Vol. 6929-8, 9-13 March

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Sherrit, Stewart (2011), Xiaoqi Bao, Christopher M. Jones, Jack B. Aldrich, Chad J. Blodget, James D. Moore, John W. Carson, and Renaud Goullioud, "Piezoelectric Multilayer Actuator Life Test", IEEE Trans. Ultrasonics, Ferroelectrics and Frequency Control. 58, no. 4, pp. 820-828

### **Acknowledgements**



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